

Solve the following questions:-

Question One (20 Mark)

1. Determine the output voltage for the circuit in Fig. 1, (6 marks)

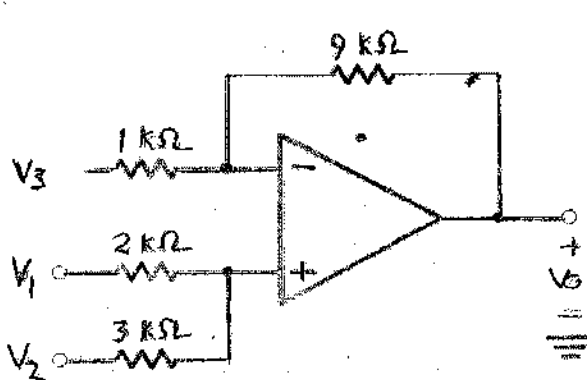


Fig . 1

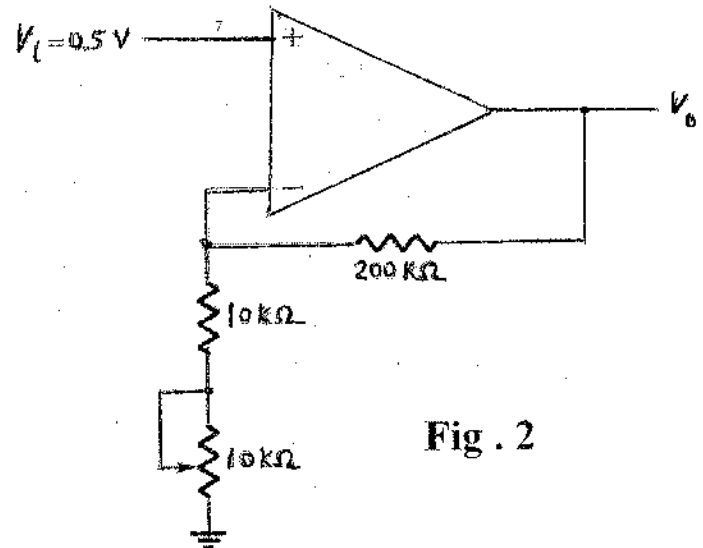


Fig . 2

2. What range of output voltage is developed in the circuit of Fig. 2 (7 marks)
 3. Define CMRR and how to experimentally measure CMRR? (7 marks)

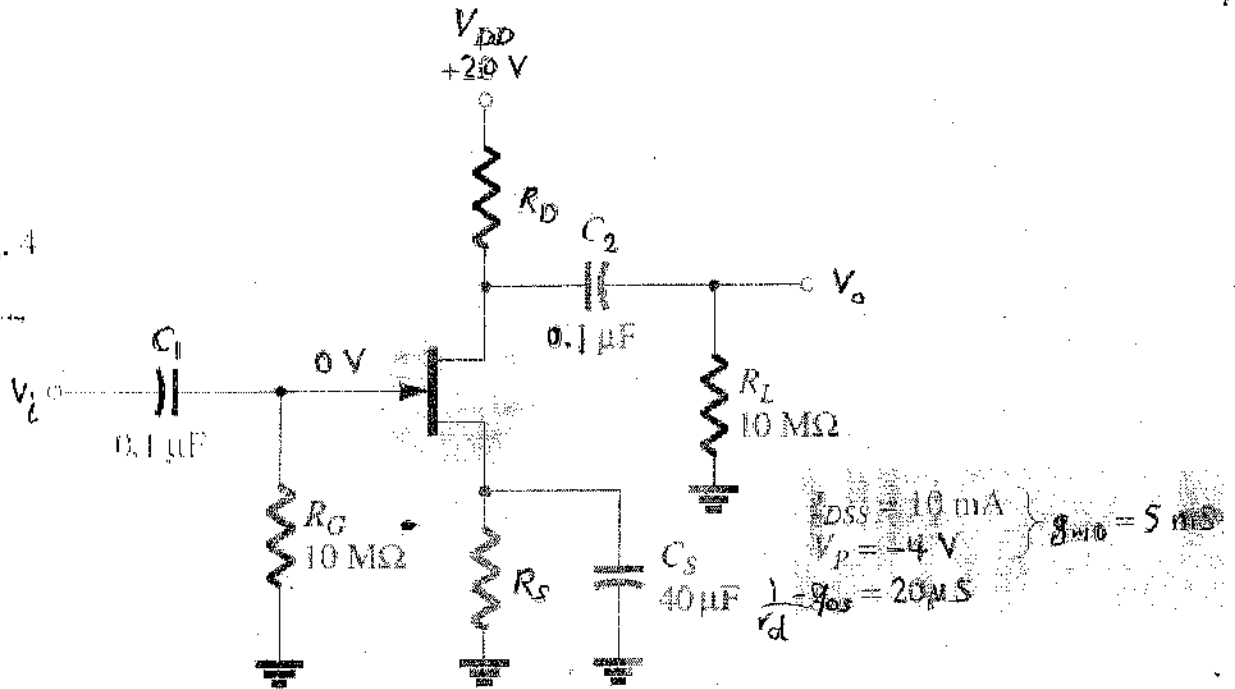
Question Two (30 Mark)

1. Calculate the efficiency of a class B amplifier for a supply voltage of $V_{CC} = 22\text{ V}$ driving a $4\ \Omega$ load with peak output voltages of: a. $V_L(p) = 20\text{ V}$. b. $V_L(p) = 4\text{ V}$.
 2. A transformer-coupled class A amplifier drives a $16\text{-}\Omega$ speaker through a $3.87:1$ transformer. Using a power supply of $V_{CC} = 36\text{ V}$, the circuit delivers 2 W to the load. Calculate:
 a. $P(ac)$ across transformer primary.
 b. $V_L(ac)$.
 c. $V(ac)$ at transformer primary.
 d. The rms values of load and primary current.
 3. Explain briefly three different configurations of practical class B power amplifier

Question Three (30 Mark)

- 1- Choose the values of R_D and R_S for the network of Fig. 3 that will result in a gain of 8 using a relatively high level of g_m for this device defined at $V_{GSQ} = 0.25V_p$.

Fig. 4



- 2- An analog switch uses an n-channel MOSFET with $V_{GS(th)} = 4$ V. A voltage of +8 V is applied to the gate. Determine the maximum peak-to-peak input signal that can be applied if the drain-to-source voltage drop is neglected.
- 3- An analog switch is used to sample a signal with $x(t) = 10 + 5\cos 2000t + 8\cos 8000t$. Determine the minimum frequency of the pulses applied to the MOSFET gate.
- 4- Design a quad time division multiplexer using an n-channel MOSFET with $V_{GS(th)} = 3$ V. A voltage of +8 V is applied to the gate of each MOSFET during $0.25 \mu s$. Calculate the sampler frequency and maximum signal frequency.



Best wishes of success
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$$V = 2 \times \frac{V_2}{5} (1+9) = 4V_2$$

$$= \frac{3V_1}{5} (1+9) = 6V_2$$

Model answer

Q1-1:

If in the circuit of Fig. E2.9 the 1-k Ω resistor is disconnected from ground and connected to a third signal source v_3 , use superposition to determine v_o in terms of v_1 , v_2 , and v_3 .

Ans. $v_o = 6v_1 + 4v_2 - 9v_3 = \underline{\underline{6V_1 + 4V_2 - 9V_3}}$

Q1-2:

$$V_o = \left(1 + \frac{R_f}{R_1} \right) V_i$$

For $R_1 = 10 \text{ k}\Omega$:

$$V_o = \left(1 + \frac{200 \text{ k}\Omega}{10 \text{ k}\Omega} \right) (0.5 \text{ V}) = 21(0.5 \text{ V}) = 10.5 \text{ V}$$

For $R_1 = 20 \text{ k}\Omega$:

$$V_o = \left(1 + \frac{200 \text{ k}\Omega}{20 \text{ k}\Omega} \right) (0.5 \text{ V}) = 11(0.5 \text{ V}) = 5.5 \text{ V}$$

V_o ranges from 5.5 V to 10.5 V.

Q1-3: Common-Mode Rejection Ratio

The ratio between A_d and A_c is the common-mode rejection ratio (CMRR),

$$\text{CMRR} = A_d / A_c$$

1. To measure A_d : Set $V_{i1} = -V_{i2} = V_s = 0.5 \text{ V}$, so that

$$V_d = (V_{i1} - V_{i2}) = (0.5 \text{ V} - (-0.5 \text{ V})) = 1 \text{ V}$$

and

$$V_c = 1/2(V_{i1} + V_{i2}) = 1/2[0.5 \text{ V} + (-0.5 \text{ V})] = 0 \text{ V}$$

Under these conditions the output voltage is

$$V_o = A_d V_d + A_c V_c = A_d (1 \text{ V}) + A_c (0) = A_d$$

Thus, setting the input voltages $V_{i1} = -V_{i2} = 0.5 \text{ V}$ results in an output voltage numerically equal to the value of A_d .

2. To measure A_c : Set $V_{i1} = V_{i2} = V_s = 1 \text{ V}$, so that

$$V_d = (V_{i1} - V_{i2}) = (1 \text{ V} - 1 \text{ V}) = 0 \text{ V}$$

$$\text{and } V_c = 1/2(V_{i1} + V_{i2}) = 1/2(1 \text{ V} + 1 \text{ V}) = 1 \text{ V}$$

Under these conditions the output voltage is

$$V_o = A_d V_d + A_c V_c = A_d (0 \text{ V}) + A_c (1 \text{ V}) = A_c$$

Thus, setting the input voltages $V_{i1} = V_{i2} = 1 \text{ V}$ results in an output voltage numerically equal to the value of A_c .

$$\text{CMRR} = A_d / A_c$$

Q2-1:

(a) $V_{L(\text{peak})} = 20 \text{ V}$

$$P_i = V_{CC} I_{dc} = V_{CC} \left[\frac{2}{\pi} \cdot \frac{V_L}{R_L} \right]$$
$$= (22 \text{ V}) \left[\frac{2}{\pi} \cdot \frac{20 \text{ V}}{4 \Omega} \right] = 70 \text{ W}$$

$$P_o = \frac{V_L^2}{2R_L} = \frac{(20 \text{ V})^2}{2(4 \Omega)} = 50 \text{ W}$$

$$\% \eta = \frac{P_o}{P_i} \times 100\% = \frac{50 \text{ W}}{70 \text{ W}} \times 100\% = 71.4\%$$

(b) $P_i = (22 \text{ V}) \left[\frac{2}{\pi} \cdot \frac{4 \text{ V}}{4 \Omega} \right] = 14 \text{ W}$

$$P_o = \frac{(4)^2}{2(4)} = 2 \text{ W}$$

$$\% \eta = \frac{P_o}{P_i} \times 100\% = \frac{2 \text{ W}}{14 \text{ W}} \times 100\% = 14.3\%$$

Q2-2

(a) $P_{pri} = P_L = 2 \text{ W}$

(b) $P_L = \frac{V_L^2}{R_L}$

$$V_L = \sqrt{P_L R_L} = \sqrt{(2 \text{ W})(16 \Omega)}$$
$$= \sqrt{32} = 5.66 \text{ V}$$

$$(c) R_2 = a^2 R_1 = (3.87)^2 (16 \Omega) = 239.6 \Omega$$

$$P_{pri} = \frac{V_{pri}^2}{R_{pri}} = 2 \text{ W}$$

$$V_{pri}^2 = (2 \text{ W})(239.6 \Omega)$$

$$V_{pri} = \sqrt{479.2} = 21.89 \text{ V}$$

$$[\text{OR, } V_{pri} = aV_L = (3.87)(5.66 \text{ V}) = 21.9 \text{ V}]$$

$$(d) P_L = I_L^2 R_L$$

$$I_L = \sqrt{\frac{P_L}{R_L}} = \sqrt{\frac{2 \text{ W}}{16 \Omega}} = 353.55 \text{ mA}$$

$$P_{pri} = 2 \text{ W} = I_{pri}^2 R_{pri} = (239.6 \Omega) I_{pri}^2$$

$$I_{pri} = \sqrt{\frac{2 \text{ W}}{239.6 \Omega}} = 91.36 \text{ mA}$$

$$\text{OR, } I_{pri} = \frac{I_L}{a} = \frac{353.55 \text{ mA}}{3.87} = 91.36 \text{ mA}$$

Solution: The operating point is defined by

$$V_{GS_0} = \frac{1}{4} V_P = \frac{1}{4} (-4 \text{ V}) = -1 \text{ V}$$

and
$$I_D = I_{DSS} \left(1 - \frac{V_{GS_0}}{V_P} \right)^2 = 10 \text{ mA} \left(1 - \frac{(-1 \text{ V})}{(-4 \text{ V})} \right)^2 = 5.625 \text{ mA}$$

Determining g_m , we obtain

$$\begin{aligned} g_m &= g_{m0} \left(1 - \frac{V_{GS_0}}{V_P} \right) \\ &= 5 \text{ mS} \left(1 - \frac{(-1 \text{ V})}{(-4 \text{ V})} \right) = 3.75 \text{ mS} \end{aligned}$$

The magnitude of the ac voltage gain is determined by

$$|A_v| = g_m (R_D \parallel r_d)$$

Substituting known values results in

$$8 = (3.75 \text{ mS})(R_D \parallel r_d)$$

so that

$$R_D \parallel r_d = \frac{8}{3.75 \text{ mS}} = 2.13 \text{ k}\Omega$$

The level of r_d is defined by

$$r_d = \frac{1}{S_{os}} = \frac{1}{20 \mu\text{S}} = 50 \text{ k}\Omega$$

and

$$R_D \parallel 50 \text{ k}\Omega = 2.13 \text{ k}\Omega$$

with the result that

$$R_D = 2.2 \text{ k}\Omega$$

which is a standard value.

The level of R_S is determined by the dc operating conditions as follows:

$$V_{GS_0} = -I_D R_S$$

$$-1 \text{ V} = -(5.625 \text{ mA}) R_S$$

and

$$R_S = \frac{1 \text{ V}}{5.625 \text{ mA}} = 177.8 \Omega$$

The closest standard value is 180Ω . In this example, R_S does not appear in the ac design because of the shoring effect of C_S .

P3-20 $V_{p-p} = 8 \text{ V}$
 P3-3 = Example $\gg 2 f_{\text{signal max}}$
 $\gg \frac{8000}{2\pi} \cdot 4$
 $f_{\text{min sample}} \geq 2.54 \text{ kHz}$

P3-4 $f_{\text{sample}} = \frac{1}{0.25 \text{ ns}} = 4 \text{ MHz}$
 $f_{\text{signal max}} = \frac{4 \text{ MHz}}{4} = 1 \text{ MHz}$

$$\frac{D}{T} = \frac{S}{f} = \frac{1}{4} \Rightarrow G = 4$$

$V_{GS} = V_G - V_S > 1$
 $V_S = V_D = V_P$
 $V_G = 8 \text{ V}$
 $8 - V_P = 4$
 $V_P = 4 \text{ V}$
 $V_{p-p} = 8 \text{ V}$