

### Model Answer

Q1-1: The magnitude of the Fresnel reflection at the fiber-air interface is

$$r = \left( \frac{n_1 - n_2}{n_1 + n_2} \right)^2 = \left( \frac{1.5 - 1}{1.5 + 1} \right)^2 = 0.04$$

The optical loss in decibels at the single interface may

$$Loss_{Fres} = -10 \log_{10}(1 - r) = -10 \log_{10}(1 - 0.04) = 0.18 \text{ dB}$$

Hence the total loss due to Fresnel reflection at the fiber joint is approximately 0.36 dB.

Q1-2: State the main inherent connection problems when jointing fibers

- (a) different core and/or cladding diameters;
- (b) different numerical apertures and/or relative refractive index differences;
- (c) different refractive index profiles;
- (d) fiber faults (core ellipticity, core concentricity, etc.).

Q1-3: Assuming uniform illumination of guided modes only, the misalignment loss may be obtained using

$$L_t = 0.85 \left( \frac{y}{a} \right) = 0.85 \left( \frac{3}{25} \right) = 0.102$$

The coupling efficiency is

$$\eta_{lat} = 1 - L_t = 1 - 0.102 = 0.898$$

Hence the insertion loss due to the lateral misalignment is

$$Loss_{lat} = -10 \log_{10} 0.898 = 0.47 \text{ dB}$$

(b) When assuming the uniform illumination of both guided and leaky modes Gloge's formula becomes:

$$L_t = 0.75 \left( \frac{y}{a} \right) = 0.75 \left( \frac{3}{25} \right) = 0.09$$

Therefore the coupling efficiency is:

$$\eta_{lat} = 1 - L_t = 1 - 0.09 = 0.91$$

and the insertion loss due to lateral misalignment is:

$$Loss_{lat} = -10 \log_{10} 0.91 = 0.41 \text{ dB}$$

Q1-4: The angular coupling efficiency is

$$\begin{aligned} \eta_{ang} &\approx \frac{16(n_1/n)^2}{(1 + n_1/n)^4} \left[ 1 - \frac{n\theta}{\pi n_1 (2\Delta)^{0.5}} \right] \\ &\approx \frac{16(n_1/n)^2}{(1 + n_1/n)^4} \left[ 1 - \frac{n\theta}{\pi NA} \right] \end{aligned}$$

For the NA = 0.2 fiber:

$$\approx \frac{16(1.48/1)^2}{(1 + 1.48)^4} \left[ 1 - \frac{5\pi}{180 \pi(0.2)} \right] = 0.797$$

The insertion loss due to the angular misalignment

$$Loss_{ang} = -10 \log_{10} 0.797 = 0.98 \text{ dB}$$

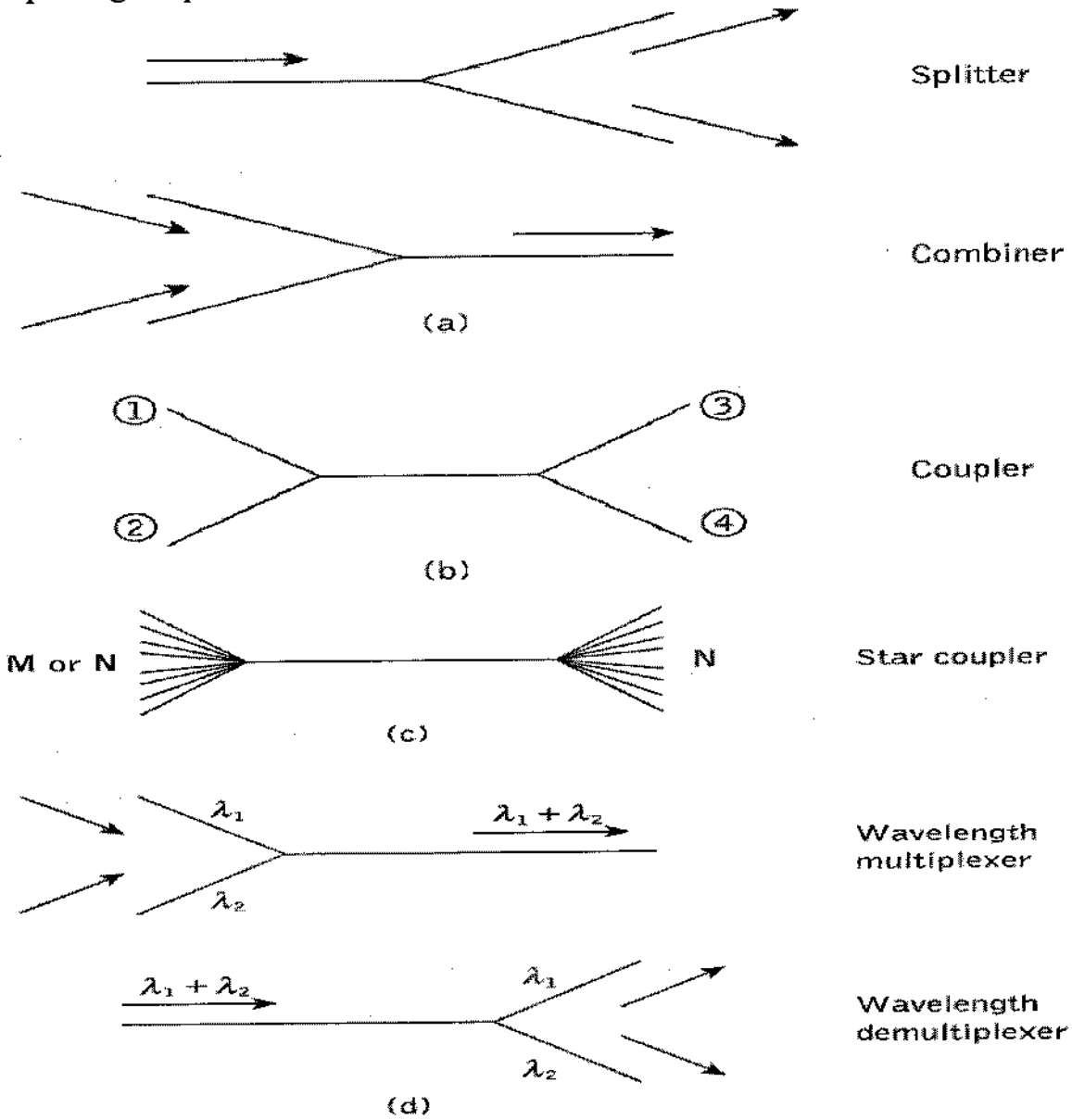
For the NA = 0.4 fiber:

$$\approx \frac{16(1.48/1)^2}{(1 + 1.48)^4} \left[ 1 - \frac{5\pi}{180} \right] = 0.862$$

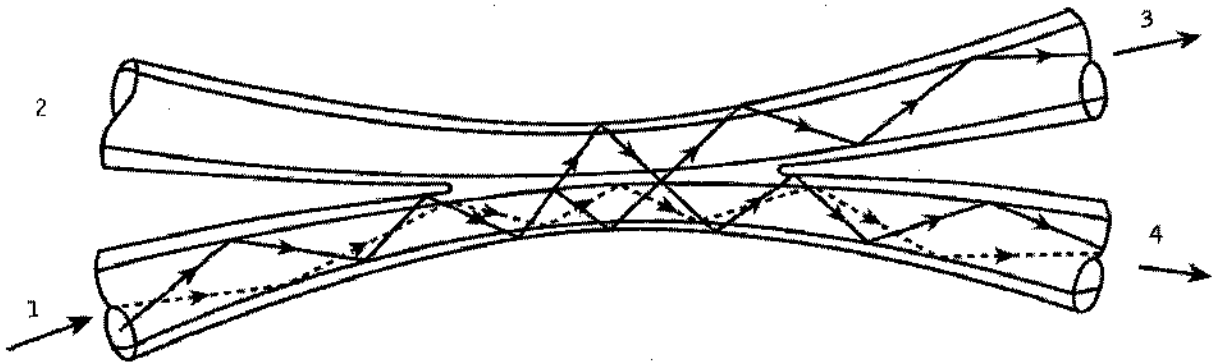
The insertion loss due to the angular misalignment

$$Loss_{ang} = -10 \log_{10} 0.862 = 0.644 \text{ dB}$$

Q1-5: Optical fiber coupler types and functions: (a) three-port couplers; (b) four-port coupler; (c) star coupler; (d) wavelength division multiplexing and demultiplexing couplers



Q2-1:



1- the excess loss is the ratio of power input to power output

$$\text{Excess loss (four-port coupler)} = 10 \log_{10} \frac{P_1}{P_3 + P_4} \text{ dB}$$

2- Insertion loss defined as the loss obtained for a particular port to-port optical path

$$\text{Insertion loss (ports 1 to 4)} = 10 \log_{10} \frac{P_1}{P_4} \text{ dB}$$

3- The crosstalk which provides a measure of the directional isolation† achieved by the device is the ratio of the backscattered power received at the second input port to the input power which may be written as:

$$\text{Crosstalk (four-port coupler)} = 10 \log_{10} \frac{P_2}{P_1} \text{ dB}$$

4- Finally, the splitting or coupling ratio indicates the percentage division of optical power between the output ports.

$$\text{split ratio} = \frac{P_3}{P_3 + P_4} \times 100 \% = \left[ 1 - \frac{P_4}{P_3 + P_4} \right] \times 100 \%$$

Q2-2:

The excess loss for the coupler

$$\text{Excess loss (four-port coupler)} = 10 \log_{10} \frac{P_1}{P_3 + P_4} \text{ dB} = 10 \log_{10} \frac{60}{53.5} = 0.5 \text{ dB}$$

$$\text{The insertion loss from 1 to 3} = 10 \log_{10} \frac{P_1}{P_3} = 10 \log_{10} \frac{60}{26} = 3.63 \text{ dB}$$

$$\text{The insertion loss from 1 to 4} = 10 \log_{10} \frac{P_1}{P_4} = 10 \log_{10} \frac{60}{27.5} = 3.39 \text{ dB}$$

$$\text{Crosstalk} = 10 \log_{10} \frac{P_2}{P_1} \text{ dB} = 10 \log_{10} \frac{0.004}{60} = -41.8 \text{ dB}$$

$$\text{split ratio} = \frac{P_3}{P_3 + P_4} \times 100 \% = \frac{26}{53.5} \times 100 = 48.6 \%$$

Q2-3

$$\text{Splitting loss} = 10 \log_{10} N = 10 \log_{10} 32 = 15.05 \text{ dB}$$

$$\text{Excess loss} = 10 \log_{10} \left( P_1 / \sum_1^N P_i \right) = 10 \log_{10} (10 / 32 \times 14) = 3.49 \text{ dB}$$

Hence the total loss for the star coupler:

total loss = splitting loss + excess loss = 15.05 + 3.49 = 18.54 dB  
 the average insertion loss from the input port to an output port is

$$\text{insertion loss} = 10 \log_{10} \frac{1000}{14} = 10 \log_{10} \frac{60}{26} = 18.54 \text{ dB}$$

Q2-4:  
 There are three main types of noise due to spontaneous fluctuations in optical fiber communication systems: thermal noise, dark current noise and quantum noise.  
 The thermal noise current  $i_t$  in a resistor R may be expressed by its mean square value

$$i_t^2 = \frac{4KTB}{R}$$

Dark current noise: When there is no optical power incident on the photodetector a small reverse leakage current still flows from the device terminals.

$$i_d^2 = 2eBI_d$$

Quantum noise

The quantum behavior of electromagnetic radiation must be taken into account at optical frequencies since  $hf > KT$  and quantum fluctuations dominate over thermal fluctuations.

Q2-5: The probability of error:

$$P(e) = \exp(-z_m) = 10^{-9}$$

and thus  $z_m = 20.7$ .

$z_m$  corresponds to an average number of photons detected in a time period  $\tau$  for a BER of  $10^{-9}$ .

$$z_m = \frac{\eta P_o \tau}{hf} = 20.7$$

Hence the minimum pulse energy or quantum limit:

$$E_{\min} = P_o \tau = \frac{20.7 hf}{\eta}$$

Thus the quantum limit at the receiver to maintain a maximum BER of  $10^{-9}$  is:

$$\frac{20.7 hf}{\eta}$$

(b) From part (a) the minimum pulse energy:

$$P_o \tau = \frac{20.7 hf}{\eta}$$

Therefore the average received optical power required to provide the minimum pulse energy is:

$$P_o = \frac{20.7hf}{\tau\eta}$$

However, for ideal binary signaling there are an equal number of ones and zeros (50% in the on state and 50% in the off state). Thus the average received optical power may be considered to arrive over two bit periods, and:

$$P_o(\text{binary}) = \frac{20.7hf}{2\tau\eta} = \frac{20.7hfB_T}{2\eta}$$

where  $B_T$  is the bit rate. At a wavelength of  $1 \mu\text{m}$ ,  $f = 2.998 \times 10^{14}$  Hz, and assuming an ideal detector,  $\eta = 1$ .

Hence:

$$P_o(\text{binary}) = \frac{20.7 \times 6.626 \times 10^{-34} \times 2.998 \times 10^{14} \times 10^7}{2}$$

$$= 20.6 \text{ pW}$$

In decibels (dB):

$$P_o \text{ in dB} = 10 \log_{10} \frac{P_o}{P_r}$$

where  $P_r$  is a reference power level.

When the reference power level is 1 watt:

$$P_o = 10 \log_{10} P_o \quad \text{where } P_o \text{ is expressed in watts}$$

$$= 10 \log_{10} 2.06 \times 10^{-11}$$

$$= 3.14 - 110$$

$$= -106.9 \text{ dBW}$$

When the reference power level is 1 milliwatt:

$$\begin{aligned}
 P_0 &= 10 \log_{10} 2.06 \times 10^{-8} \\
 &= 3.14 - 80 \\
 &= -76.9 \text{ dBm}
 \end{aligned}$$

Q3-

*[Handwritten notes on a grid background, partially obscured by a dark shadow. The text is difficult to read but appears to contain technical details related to a system design or analysis.]*

$P_{3-dB} = 1.5 \text{ dB}$  (19) 90.10  
 mode = DR2  
 fiber = 100 m  
 sources = 1000 pW  
 2 m  
 1 ns  
 1 dB  
 system measurement  
 BER = 10<sup>-9</sup>  
 BR = 10 Gbps  
 system rise time  
 attenuation = 20 dB/km  
 $\alpha_f = 2 \text{ dB/km}$   
 $\alpha_c = 2 \text{ dB/km}$   
 system length  
 100 m  
 $\alpha_{sp} = 7 \text{ dB/km}$   
 12.5 m

The value is difficult to satisfy  
 with source matching = 200  
 The output is 1.1  

$$= 1.1 \sqrt{1 + (100)^2} + (100)^2$$
 So

Let's get the actual system  
 must be 3.8  

$$= 1 \text{ ps}$$

yes, assume  
 but not  

$$= 2 \text{ ps}$$

$V_{rms} = 10^{-10}$   
 $(\frac{10}{10}) = 10^{-10}$  32 dBm

total loss margin = source - P<sub>in</sub> - P<sub>out</sub>  
 source = 30 dBm  
 $P_{in} = 10 \log_{10} \frac{50000 \times 10^{-10}}{1} = 19.9$   
 $\approx 20$  dBm

then total loss margin = 7 - (-53.5) = 60.5 dBm

rx power = total loss margin - total attenuation  
 $60.5 - 26.7 = 33.4$  dBm

actual power at Rx = P<sub>in</sub> + margin  
 $19.9 + 33.4 = 53.3$  dBm

defining actual = 100  
 $\frac{P_{actual}}{P_{nom}} = 10^{\frac{53.3 - 10}{10}} = 10^{4.33} = 21.5$  Max

$2K = 10 \log_{10}(K^2) = -6$   
 $K^2 = 10^{-0.6} = 0.275$   
 $K = 0.52$   
 $FAP = 10 \log_{10}(0.52)(10)$

52.5 dB  
 get the value  
 these min  
 (8)



Q3-d

$$(4.) R = \frac{\eta e}{hf} = \frac{0.8 * 1.602 * 10^{-19} * 1.3 * 10^{-6}}{6.626 * 10^{-34} * 3 * 10^8} = 0.8371 \text{ Aw}^{-1}$$

$$K = 10^{\text{SNR(dB)}/10} = 10^{2.2} = 158.49$$

$$P_{\min} = \frac{2eFK^2\Delta F}{R} = \frac{2(1.6e-19)(1)(158.49)(25e9)}{0.8371}$$

$$= 1.515 \text{ } \mu\text{w}$$

$$\text{In dBm} \quad P_{\min} = 10 \log_{10} \left( \frac{P_{\min}}{1 \text{ mW}} \right) = -28.1967 \text{ dBm}$$

\* Fiber type : Single mode fiber

because long distance  $> 1 \text{ Km}$  and high speed  $> 1 \text{ Gbps}$

\* Power budget analysis :

① total fiber atten. =  $15 * 0.2 = 3 \text{ dB}$

② No. of splices = 29

Splices atten. =  $29 * 0.1 = 2.9 \text{ dB}$

③ Connector loss =  $2 * 1 = 2 \text{ dB}$

④ Source average power =  $7 \text{ dBm}$

$$\boxed{5} \text{ time degradation factor loss} = 3 \text{ dB}$$

$$\boxed{6} \text{ environment degradation factor} = 5 \text{ dB}$$

$$\boxed{7} \text{ total atten.} = 3 + 2.9 + 2 + 3 + 5 \\ = 15.9 \text{ dB}$$

$$\boxed{8} \text{ total loss margin} = \text{Source av.} - \text{Receiver sen.} \\ = 7 \text{ dB} - (-28.197) \\ = 35.197 \text{ dBm}$$

$$\boxed{9} \text{ Excess power} = \text{total loss margin} - \text{total atten.} \\ = 35.197 - 15.9 = 19.297 \text{ dBm}$$

$$\boxed{10} \text{ Actual power at Receiver} \\ = \text{Receiver sensitivity} + \text{excess power} \\ = -28.1967 + 19.297 = -8.9 \text{ dBm}$$