



Please, answer the following questions (assume any missing data):-

١- The following details refer to a water centrifugal pump. The impeller outer diameter is ٣٠ cm in diameter and its inlet diameter is ١٥ cm. The impeller width at outlet is ٢ cm. The blade angle at inlet is ٣٠° and at outlet is ٢٥°. The impeller speed is ١٤٥٠ rpm. The impeller is designed for constant flow velocity through the impeller and for no-whirl at inlet. The input shaft power is ٢٦.٥ kW and the overall efficiency is ٧٦%. Determine: the width of the impeller at inlet and the theoretical head developed by this impeller (١٥ Marks)

$$U_1 = \frac{2\pi Nr_1}{60} = \frac{2\pi \times 1450 \times 7.5}{60 \times 100} = 11.38 \text{ m/s}, \quad U_2 = \frac{2\pi Nr_2}{60} = \frac{2\pi \times 1450 \times 15}{60 \times 100} = 22.76 \text{ m/s}$$

$$Q = 2\pi r_1 b_1 C_{r1} = 2\pi r_2 b_2 C_{r2} \quad \therefore C_{r1} = C_{r2}$$

$$\therefore r_1 b_1 = r_2 b_2 \quad 15 \times b_2 = 30 \times 2 \quad b_1 = 4 \text{ cm}$$

for no whirl at inlet: $C_{x1} = 0 \quad \therefore \tan 30^\circ = \frac{C_{r1}}{U_1} = \frac{1}{\sqrt{3}} = \frac{C_{r1}}{11.38} \quad \therefore C_{r1} = 6.575 \text{ m/s}$

$$\therefore Q = 2\pi r_1 b_1 C_{r1} = 2\pi \times 0.04 \times 0.075 \times 6.575 = 0.12394 \text{ m}^3/\text{s}$$

$$\therefore \eta = \frac{\rho g Q H}{P_m} = \frac{1000 \times 9.81 \times 0.12394 \times H}{26.5 \times 1000} = 0.76 \quad \therefore H = 16.56 \text{ m}$$

$$H_{th} = \frac{1}{g} (U_2 C_{x2}) \quad , C_{x2} = U_2 - C_{r2} \cot \beta_2 = U_2 - C_{r1} \cot \beta_2$$

$$\therefore C_{x2} = 22.76 - 6.575 \times \cot 25^\circ = 8.66 \text{ m/s},$$

$$H_{th} = \frac{1}{g} (U_2 C_{x2}) = \frac{1}{9.81} \times 22.76 \times 8.66 = 20.1 \text{ m}$$

٢- A centrifugal pump has the following characteristics at ١٠٠٠ rpm:

Q (m ^٣ /h)	٠	٢٣	٤٦	٦٩	٩٢	١١٥
H (m)	١٧	١٦	١٣.٥	١٠.٥	٦.٦	٢
Eff (%)	٠	٤٩.٥	٦١	٦٣.٥	٥٣	١٠

The pump is used to pump water from a low reservoir to a high reservoir through a total length of ٨٠٠ m of pipe ١٥ cm in diameter. The difference between the water levels in the reservoirs is ٨ m. considering only frictional losses where the friction factor is ٠.٠١٦. Find the rate of flow between the reservoirs. Also determine the power input to the pump.

If the pump speed is reduced to ٨٠٠ rpm, deduce all new performance data plus the input power performance and plot them in addition to the power curve. Also, determine the new operating point and the power. Identify the power consumed at zero discharge. (٢٠ Marks)

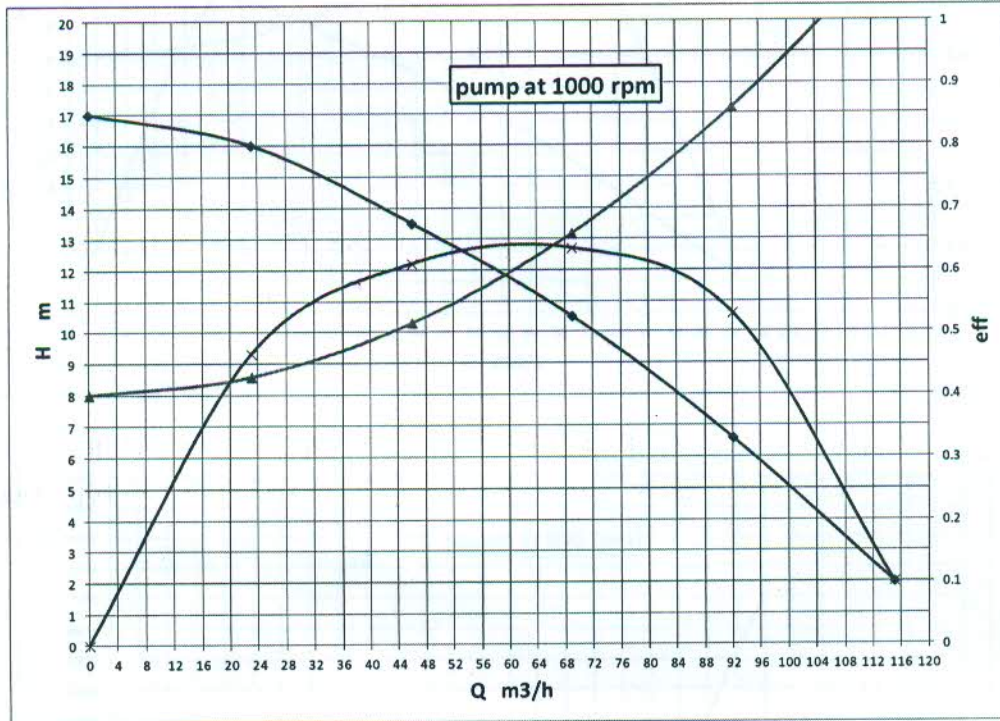
a- The system eq is: $H = \lambda + (0.016 * \lambda^{0.1} / 0.10 + 1)(Q^2 / 2ga^5)$

$$a = 3.14 / \pi (0.10)^2 = 0.01767 \text{ m}^2$$

$$H = \lambda + 14.9077 * Q^2$$

From the drawing the operating point is: $Q = 68.0 \text{ m}^3/\text{h}$, $H = 11.7 \text{ m}$, $\text{eff} = 0.64$

The required power = $9810 * 68.0 * 11.7 / (0.64 * 3600 * 1000) = 2.914 \text{ kW}$



b- from similarity laws:

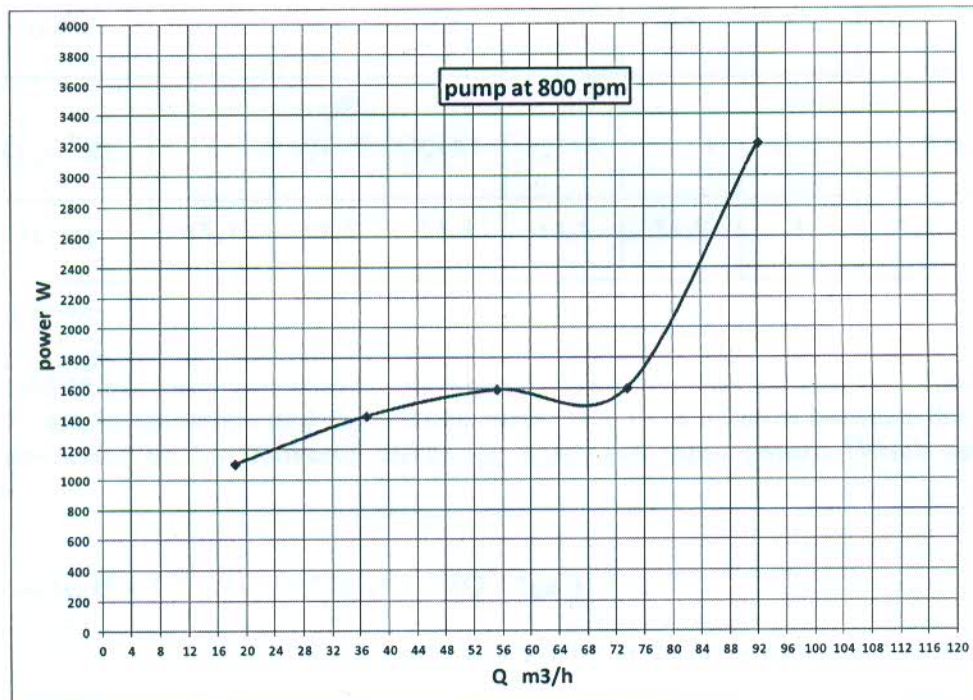
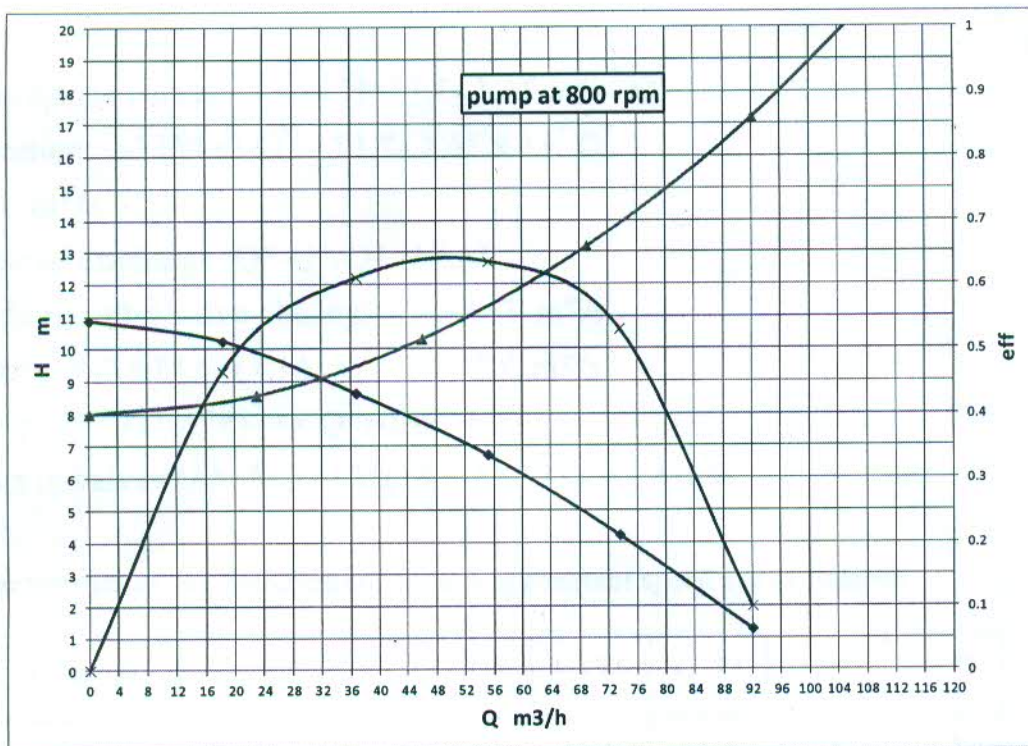
$$Q_{\lambda..} = 0.8 Q_{1000}$$

$$H_{\lambda..} = 0.64 H_{1000}$$

$$P_{\lambda..} = 0.512 P_{1000}$$

The new performance table at 800 rpm:

Q (m ³ /h)	0	18.4	36.8	55.2	73.6	92
H (m)	10.88	10.24	8.64	7.04	5.44	4.28
Eff (%)	0	49.0	61	63.0	53	10
Power (kW)		1.104	1.42	1.091	1.098	3.208



The required power = $9.81 \times 32.0 \times 9.2 / (0.98 \times 3600 \times 1000) = 1.08 \text{ kW}$

Power at zero discharge by extrapolating the power curve to cut the power axis at 0 discharge.

Then P at 0 $Q \sim 1.0 \text{ kW}$

- 3- (a) $1.0 \text{ m}^3/\text{s}$ of water flows from tank A to tank B due to a difference of water level of 6 m . In order to increase this discharge, a booster pump is used in the line. Calculate the percentage increase in discharge. The performance of the pump is given by $H = 31.3 - 1.83 \times 10^{-3} Q^2$.
- (b) If a valve, located on the discharge side of the pump, is partially closed to reduce the discharge by 10% , how much power lost in the valve. (10 Marks)

The system curve : $H = -7 + 2.5 \times 10^{-5} Q^2$

The performance curve: $H = 31.3 - 1.83 \times 10^{-5} Q^2$

At intersection: $-7 + 2.5 \times 10^{-5} Q^2 = 31.3 - 1.83 \times 10^{-5} Q^2$

$$Q = 0.094 \text{ m}^3/\text{s}$$

$$\% \text{ increase of discharge} = \frac{Q_2 - Q_1}{Q_1} = 87.8\%$$

New discharge after valve closing: $0.0847 \text{ m}^3/\text{s}$

$$H \text{ by system} = -7 + 2.5 \times 10^{-5} (0.0847)^2 = 11.177 \text{ m}^3/\text{s}$$

$$H \text{ by pump} = 31.3 - 1.83 \times 10^{-5} (0.0847)^2 = 18.2 \text{ m}^3/\text{s}$$

$$\text{Power lost in valve} = 9.81 \times 0.0847 \times (18.2 - 11.177) = 0.8 \text{ kW}$$

4- The characteristics of two rotodynamic pumps at constant speed are as follows:

Pump A

Q (m ³ /s)	0	0.006	0.012	0.018	0.024	0.03	0.036
H (m)	22.6	21.9	20.3	17.7	14.2	9.7	3.9
Eff (%)	0	32	74	86	80	66	28

Pump B

Q (m ³ /s)	0	0.006	0.012	0.018	0.024	0.03	0.036
H (m)	16.2	13.6	11.9	11.6	10.7	9	6.4
Eff (%)	0	14	34	60	80	80	60

If they are used to lift water continuously through 3.2 m of vertical lift and the pipe to be used is 21 m long, 10 cm in diameter, and the friction factor is 0.02. Compare between the operation of the two pumps based on the delivered discharge, head, and input power. Which one would you prefer to use?

(20 Marks)

The system eq is: $H = 3.2 + (0.02 \times 21 / 0.1 + 1)(Q^2 / 2ga^5)$

$$a = 3.14 / 4 (0.1)^2$$

$$H = 3.2 + 4296.6 \times Q^2$$

From the drawing the operating point for pump A:

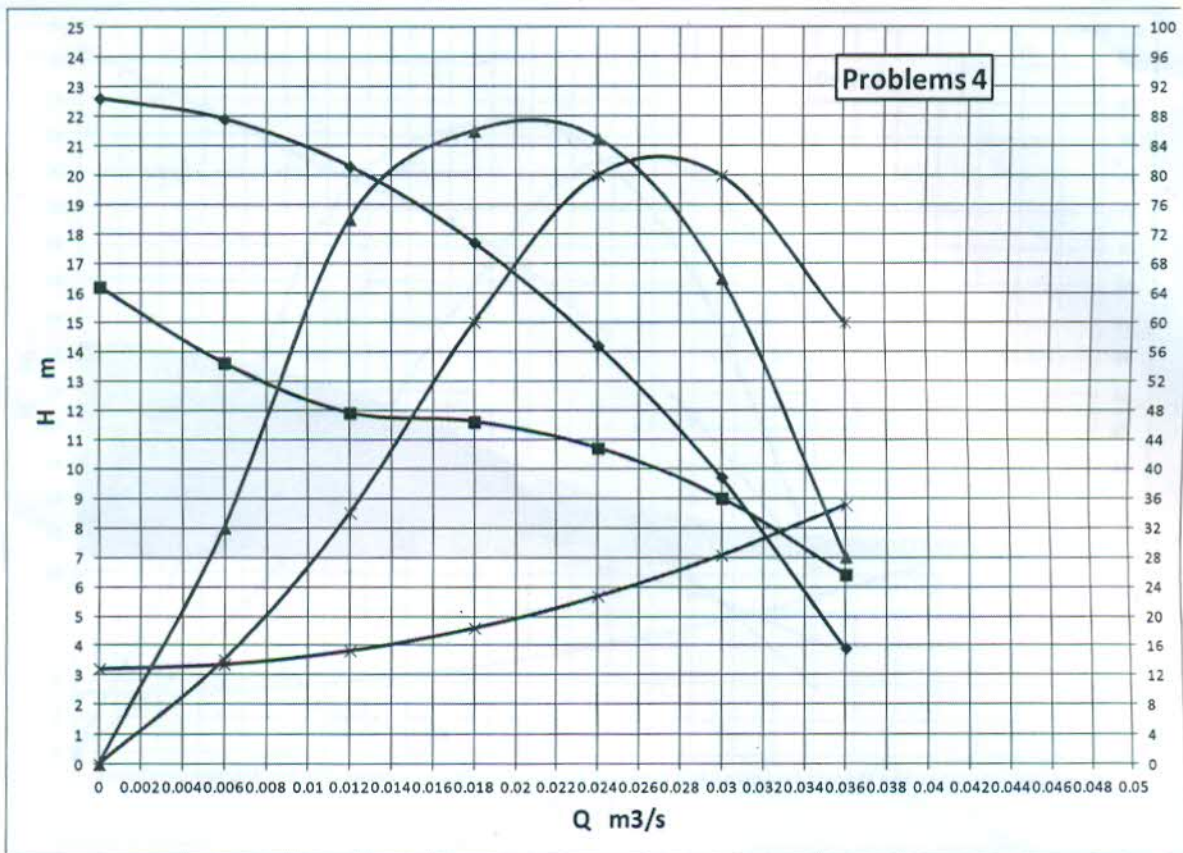
$$Q = 0.032 \text{ m}^3/\text{s}, \quad H = 7.7 \text{ m}, \quad \text{eff} = 0.00$$

From the drawing the operating point for pump B:

$$Q = 0.033 \text{ m}^3/\text{s}, \quad H = 7.9 \text{ m}, \quad \text{eff} = 0.72$$

$$\text{The required power} = 9.81 \times 0.032 \times 7.7 / (0.00 \times 1000) = 4.4 \text{ kW}$$

$$\text{The required power} = 9.81 \times 0.033 \times 7.9 / (0.72 \times 1000) = 3.0 \text{ kW}$$



o- If the pumps in problem (4) are used one time in series and another time in parallel, plot both characteristics curves for the two combinations. Determine the consumed power by the pumps in the two cases. (10 Marks)

Series connections:

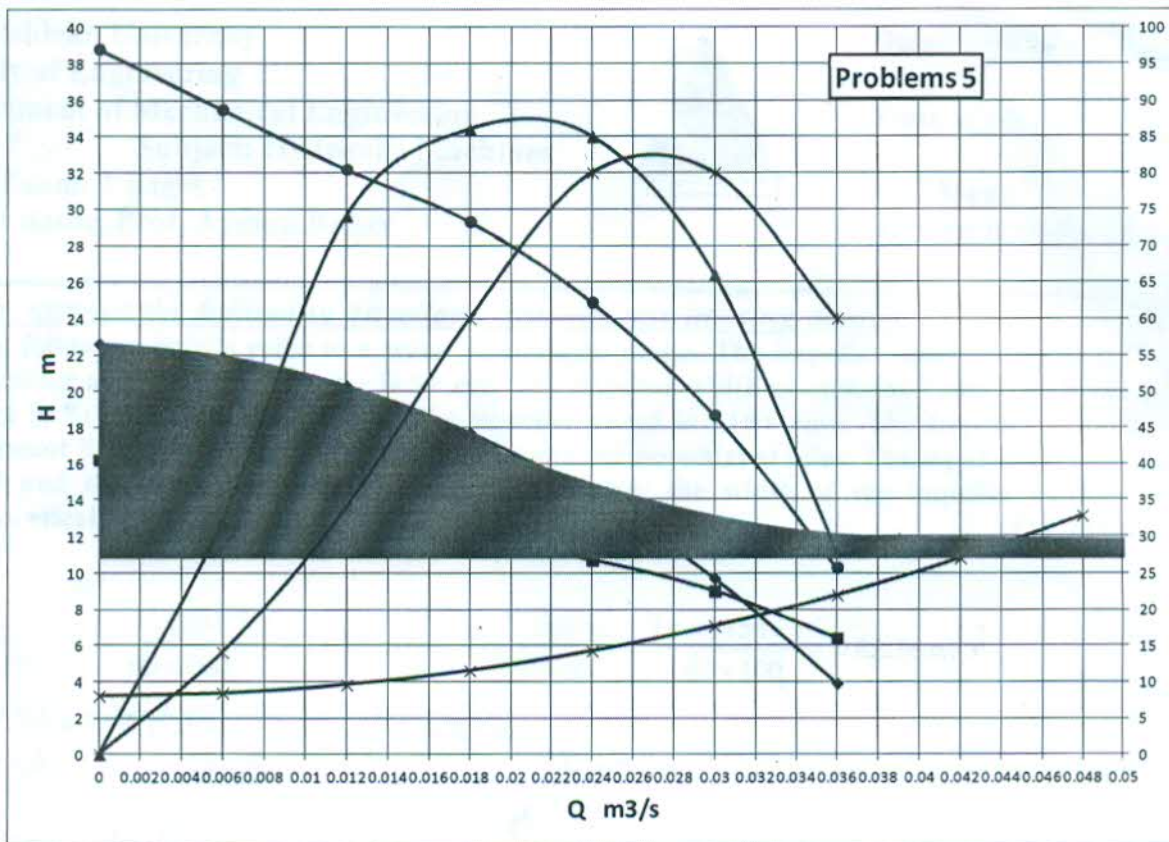
$Q_A = 0.037 \text{ m}^3/\text{s}, \quad H_A = 3 \text{ m}, \quad \text{eff A} = 0.22$

$Q_B = 0.037 \text{ m}^3/\text{s}, \quad H_B = 6 \text{ m}, \quad \text{eff B} = 0.07$

Parallel connections:

$Q_A = 0.027 \text{ m}^3/\text{s}, \quad H_A = 12 \text{ m}, \quad \text{eff A} = 0.78$

$Q_B = 0.018 \text{ m}^3/\text{s}, \quad H_B = 12 \text{ m}, \quad \text{eff B} = 0.6$



- ٦- Do the pumps in problem (٤) operate free of or with cavitation? The suction pipe is ٧ m long with the same pipe. The suction static lift is ١.٥ m. If the water temperature is ٢٥°C ($p_v = ٣.٣$ kPa abs and water density = ٩٩٧ kg/m^٣) and the atmospheric pressure is ١٠١ kPa. Consider the Thoma cavitation factor as ٠.٢٥. (١٠ Marks)

For pump A:

$$NPSH_r = 0.25 \times 7.7 = 1.925 \text{ m}$$

$$NPSH_a = 10.32 - 1.5 - 1.354 - 0.337 = 7.129 \text{ m}$$

The pump A is save of cavitation

For pump B:

$$NPSH_r = 0.25 \times 7.9 = 1.975 \text{ m}$$

$$NPSH_a = 10.32 - 1.5 - 1.44 - 0.337 = 7.043 \text{ m}$$

The pump B is save of cavitation

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